## **REMARKS/ARGUMENTS**

Favorable reconsideration of this application in light of the following discussion is respectfully requested.

Claims 1-13 are presently pending in this application, Claim 13 having been newly added by the present amendment.

In the outstanding Office Action, Claims 6 and 9-12 were rejected under 35 U.S.C. §102(b) as being anticipated by <u>Jullian et al.</u> (U.S. Patent 5,863,315); and Claims 1-5, 7 and 8 were rejected under 35 U.S.C. §103(a) as being unpatentable over <u>Jullian et al.</u> in view of <u>Kulprathipanja</u> (U.S. Patent 5,900,523).

Newly added Claim 13 is believed to find clear support in the specification, claims and drawings as originally filed. For example, Claim 13 is believed to be supported by Claim 1 and page 4, lines 19-21, describing that the adsorptions are carried out preferably at a temperature of from 20 to 180°C and at a pressure of from 1 to 10 bar, and pages 6-7, describing that the experimental tests are carried out at a temperature of about 160°C and at a pressure of about 1.1 bar.

Briefly recapitulating, Claim 6 of the present application is directed to a process for separating mixtures of hydrocarbon isomers in gas phase on molecular sieves, and the process includes the steps of providing a plurality of columns each including molecular sieves and configured to function alternately such that the columns are designated to function from a secondary adsorption device, to a primary adsorption device, and to a desorption device in sequence, feeding the mixtures of hydrocarbon isomers to at least one of the columns functioning as the primary adsorption device such that isomers with a greater selectivity towards the molecular sieves in the mixtures of hydrocarbon isomers are adsorbed, feeding an

entire effluent of the mixtures of hydrocarbon isomers from the at least one of the columns functioning as the primary adsorption device to at least one of the columns functioning as the secondary adsorption device such that remaining of the isomers with a greater selectivity towards the molecular sieves are adsorbed, discharging isomers with a lower selectivity towards the molecular sieves in the mixtures of hydrocarbon isomers from the at least one of the columns functioning as the secondary adsorption device and a desorbing agent remaining therein, feeding a desorbing agent to at least one of the columns functioning as the desorption device, discharging isomers with a greater selectivity towards the molecular sieves in the mixtures of hydrocarbon isomers and the desorbing agent in the at least one of the columns functioning as the desorption device, and rotating the columns from the secondary adsorption device, to the primary adsorption device, and to the desorption device in sequence.

The outstanding Office Action asserts that <u>Jullian et al.</u> disclose the process as recited in Claim 6. However, <u>Jullian et al.</u> are not believed to teach "feeding an *entire* effluent of the mixtures of hydrocarbon isomers from the at least one of the columns functioning as the primary adsorption device to at least one of the columns functioning as the secondary adsorption device such that remaining of the isomers with a greater selectivity towards the molecular sieves are adsorbed; ... and rotating the columns from the secondary adsorption device, to the primary adsorption device, and to the desorption device in sequence" as recited in Claim 6 (emphasis added in Italic). On the other hand, in the <u>Jullian et al.</u> process, only a portion of the effluent is extracted to conduct the second pressurization step. <sup>1</sup> In addition, the adsorption phase is performed in only one column. It is thus respectfully submitted that the process recited in Claim 6 is believed to be distinguishable from <u>Jullian et al.</u>

<sup>&</sup>lt;sup>1</sup> See <u>Jullian et al.</u>, column 3, lines 60-64.

Turning now to Claim 1, Claim 1 of the present invention is directed to a process for separating mixtures of hydrocarbon isomers in gas phase on molecular sieves, and the process includes the steps of providing a plurality of columns each including molecular sieves and configured to function alternately such that the columns are designated to function from a secondary adsorption device, to a primary adsorption device, and to a desorption device in sequence, feeding the mixtures of hydrocarbon isomers to at least one of the columns functioning as the primary adsorption device such that isomers with a greater selectivity towards the molecular sieves in the mixtures of hydrocarbon isomers are adsorbed, feeding an entire effluent of the mixtures of hydrocarbon isomers from the at least one of the columns functioning as the primary adsorption device to at least one of the columns functioning as the secondary adsorption device such that remaining of the isomers with a greater selectivity towards the molecular sieves are adsorbed, discharging isomers with a lower selectivity towards the molecular sieves in the mixtures of hydrocarbon isomers from the at least one of the columns functioning as the secondary adsorption device and a desorbing agent remaining therein, feeding a desorbing agent to at least one of the columns functioning as the desorption device, discharging isomers with a greater selectivity towards the molecular sieves in the mixtures of hydrocarbon isomers and the desorbing agent in the at least one of the columns functioning as the desorption device, feeding the isomers with a lower selectivity towards the molecular sieves and the desorbing agent discharged from the at least one column functioning as the secondary adsorption device to a first distillation unit configured to recover the desorbing agent for recycling for the at least one column functioning as the desorption device, feeding the isomers with a greater selectivity towards the molecular sieves and the desorbing agent discharged from the at least one of the columns functioning as the desorption device to a second distillation unit configured to recover the desorbing agent for recycling for the at

least one of the columns functioning as the desorption device, and rotating the columns from the secondary adsorption device, to the primary adsorption device, and to the desorption device in sequence. By feeding the mixture of hydrocarbon isomers and rotating the columns as such, one cycle of the columns in the process is conducted in only three phases, thereby achieving a simplified system with a higher adsorption yield of the extracted product.

The outstanding Office Action asserts that the process as recited in Claim 1 is obvious from Jullian et al. and Kulprathipanja. However, it is respectfully submitted that the combination of these cited references is believed to be improper. Specifically, Jullian et al. disclose a process for separating hydrocarbons mixtures wherein the hydrocarbon mixture is sent to an adsorption zone in vapour phase, while Kulprathipanja discloses a process for separating metaxylene from a mixture of C<sub>8</sub> aromatic hydrocarbons in which the mixture is sent to an adsorption zone in liquid phase. These two references differ in the phase of the adsorption step (vapour phase versus liquid phase). It is thus believed to be inappropriate to modify the Jullian et al. process by adding a step (namely the separation of the desorbing agent) of the Kulprathipanja process that carries out the adsorption with a different phase. Furthermore, in the Kulprathipanja process, the desorbing agent is not present in the feed mixture. On the other hand, Jullian et al. disclose the process in which the desorbing agent, consisting of isobutane, n-butane, isopentane and n-pentane, is already present in the feed charge and it is an integral part of the separated product.<sup>2</sup> Therefore, there is no reason to submit it to a separation to use it again in the system, i.e., it has no meaning at all to submit the obtained product to any separation when the desorbing agent to be separated is the same component of the wished mixture, and the combination of these processes is believed to be improper. Even assuming arguendo that Jullian et al. and Kulprathipanja are combined, the

<sup>&</sup>lt;sup>2</sup> See id., examples 1 and 2.

combined teachings are not believed to render the process recited in Claim 1 obvious, since the adsorbing and desorbing in the process of Claim 1 are performed without pressure change. For example, in the examples 1-4 presented in the Applicants' specification, the experimental tests are carried out at a temperature of about 160°C and at a pressure of about 1.1 bar. In the examples 5-6, the laboratory unit is placed in an oven to maintain the temperature of about 160°C required by the experimentation. It is thus clear that both temperature and pressure are maintained constant during the entire process. In contrast, according to Jullian et al., each column during the nine phases is first pressurized, then depressurized and then again pressurized.<sup>3</sup> Furthermore, significant differences from <u>Jullian</u> et al. are clearly shown by the comparison data provided in Attachments A-C. In the two examples of Jullian et al., a recovering of i-paraffin equal to 59.4% and 56.7% with a title respectively equal to 88.6 and 87.1% is obtained, while in the example according to the process of Claim 1, a recovery of ethylbenzene of 56% with a title of 99.9% is obtained. It is therefore evident from these data that the process according to Claim 1 of the present application allows one to obtain a purer product. Therefore, the process recited in Claim 1 is believed to be distinguishable from Jullian et al. and Kulprathipanja.

Likewise, independent Claim 13 includes subject matter substantially similar to what is recited in Claim 13 to the extent discussed above. Thus, Claim 13 is also distinguishable from Jullian et al. and Kulprathipanja.

For the foregoing reasons, Claims 1, 6 and 13 are believed to be allowable. Furthermore, since Claims 2-5 and 7-12 depend ultimately from either Claim 1 or 6, substantially the same arguments set forth above also apply to these dependent claims. Hence, Claims 2-5 and 7-12 are believed to be allowable as well.

<sup>&</sup>lt;sup>3</sup> See id., column 17, lines 4-46.

Application No. 09/886,994 Reply to Office Action of August 27, 2003

In view of the amendments and discussions presented above, Applicants respectfully submit that the present application is in condition for allowance, and an early action favorable to that effect is earnestly solicited.

Respectfully submitted,

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## Attachment A

Example 1, Jullian et al.

4 columns

12 sequences

		%9.88	11.4%												
REF		12.551	1.619	14.170					80.1%	19.9%					59.4% 88.6%
MIX		14.635	5.015				MIX+DES		21.140	5.250	26.390				l-paraffin
		1-paraff	n-paraff						l-paraff	n-paraff					Recovery Title
EXTRACTED	Kg/h	0.372	0.200	6.537	2.047	0.422	0.179	0.543	0.322	1.115	0.075	0.213	0.194	-	12.22
	d%	3.05	1.64	53.50	16.75	3.45	1.47	4.45	2.64	9.12	0.61	1.74	1.59		100.00
REFINED	Kg/h	0.187	0.229	5.181	0.160	1.799	0.764	2.326	1.387	0.084	0.318	0.907	0.828		14.17
	d%	1.32	1.61	36.49	1.13	12.67	5.38	16.38	6.77	0.59	2.24	6.39	5.83		99.80
MIX	Kg/h	0.273	0.200	5.500	2.201	2.220	0.943	2.869	1.710	1.199	0.393	1.120	1.022		19.65
	d%	1.39	1.02	27.99	11.20	11.30	4.80	14.60	8.70	6.10	2.00	5.70	5.20	,	100.00
DES	Kg/h	0.286	0.228	6.218	0.007		•								6.74
	d%	4.25	3.39	92.26	0.10										100.00

Example 2, Jullian et al.

3 columns

9 sequences

		87.1%	12.9%													
REF		11.991	1.779	13.774					80.1%	19.9%						56.7% 87.1%
MIX		14.635	5.015				MIX+DES		21.140	5.250	26.390					l-paraffin
		1-paraff	n-paraff						l-paraff	n-paraff						Recovery Title
ACTED	Kg/h	0.314	0.249	6.750	1.870	0.523	0.222	0.675	0.401	1.018	0.093	0.264	0.241	,		12.62
EXTRACT	d%	2.57	2.03	55.24	15.30	4.28	1.18	5.53	3.28	8.33	0.76	2.16	1.97			103.27
REFINED	Kg/h	0.245	0.180	4.968	0.337	1.698	0.722	2.194	1.308	0.180	0.300	0.856	0.781			13.77
	d%	1.78	1.31	36.08	2.45	12.33	5.24	15.93	9.50	1.31	2.18	6.22	2.67			100.00
MIX	Kg/h	0.273	0.200	5.500	2.201	2.220	0.943	2.869	1.710	1.199	0.393	1.120	1.022			19.65
	d%	1.39	1.02	27.99	11.20	11.30	4.80	14.60	8.70	6.10	2.00	5.70	5.20			 100.00
DES	Kg/h	0.286	0.228	6.218	0.007										•	 6.74
	d%	4.25	3.39	92.26	0.10											100.00

Attachment C

Example according to the application in re

3 columns

3 sequences (phases)

	%6.66	0.1%			
REF	13.744	$\frac{0.014}{13.758}$		93.0%	%6.00% 99.9%
MIX	24.543	1.847	MIX+DES	24.543 1.847 26.390	
	Ethylbenzene	P-xilene		Ethylbenzene P-xilene	Recovery Ethylbenzene Title
CTED	Kg/h 10.799	1.834		31 AUG	12.63233
EXTRACTED	%p 85.5%	14.5%			100.0%
VED	Kg/h 13.744	0.014			13.758
REFINED	%6.66 9%	0.1%		·	100.0%
	Kg/h 24.543	1.847			26.39
MIX	%b 93.0%	7.0% 0.0%			100.0%
	Kg/h				 6.74
DES	%p 00.00	0.00			100.00

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